



17<sup>TH</sup> ADVANCED BEAM DYNAMICS WORKSHOP ON

## **FUTURE LIGHT SOURCES**

# **Development of Variable Polarization Undulators for ELETTRA**

*B. Diviacco, Sincrotrone Trieste*

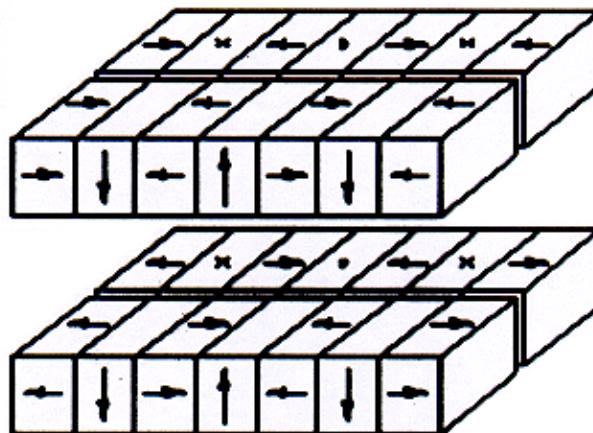
APRIL 6-9, 1999

ARGONNE NATIONAL LABORATORY, ARGONNE, IL U.S.A.

# Development of Variable Polarization Undulators for ELETTRA

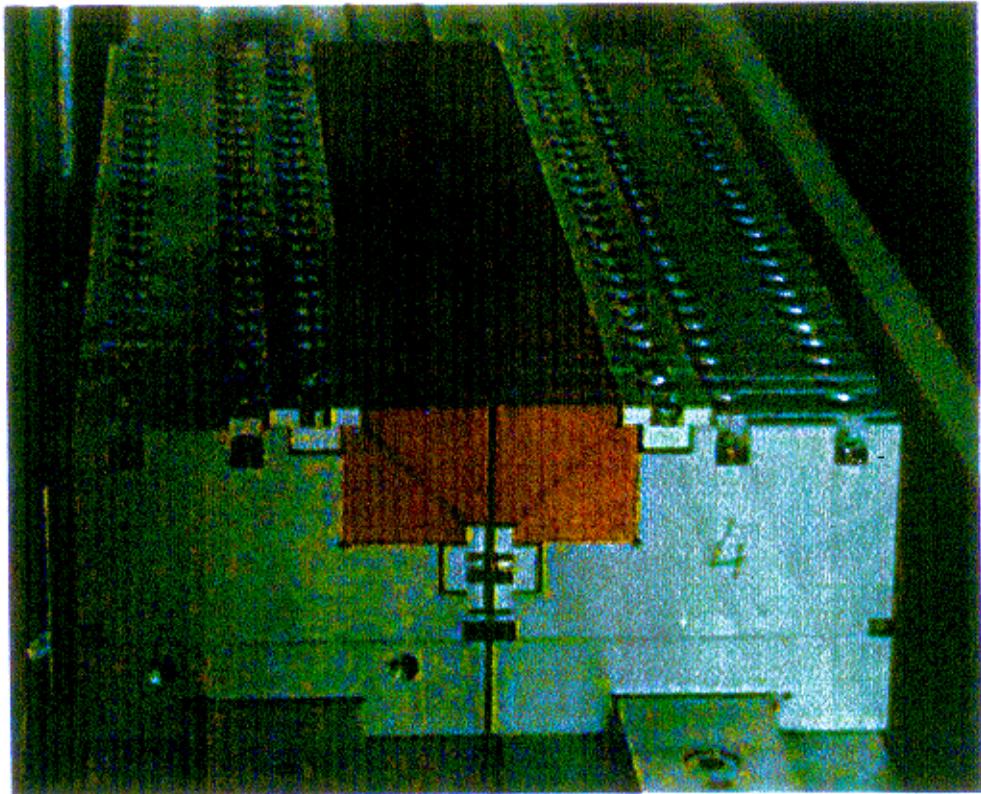
B. Diviacco – Sincrotrone Trieste

- An APPLE type structure has been chosen for the next 6 Elettra undulators

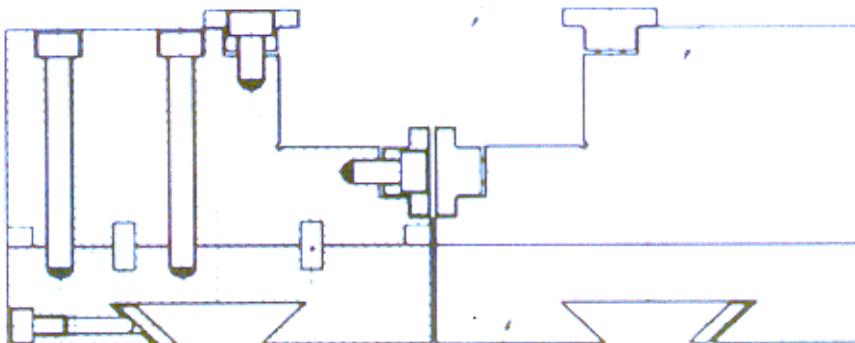


period (mm)	Np	Horizontal Polarization		Circular Polarization		Vertical Polarization	
		B <sub>0</sub> (T)	ε <sub>1</sub> (eV)	B <sub>0</sub> (T)	ε <sub>1</sub> (eV)	B <sub>0</sub> (T)	ε <sub>1</sub> (eV)
48	44	0.57	185	0.29	294	0.33	371
60	36	0.78	59	0.42	94	0.51	123
77	28	0.91	22	0.53	32	0.65	42
100	20	1.01	8	0.63	10	0.78	12
125*	17	0.78	8	0.47	10	0.60	12

\* quasi-periodic



Blocks and block holders:



Magnetic material :	NdFeB (die-pressed)
Remanent field:	1.33 T
Dipole moment:	$\pm 0.5\%$
Angle:	$\pm 0.7^\circ$
$\mu_{  }$ :	1.05
$\mu_\perp$ :	1.15

*Is there an improvement in magnet block quality (homogeneity) observable over the last years ?*

	typical N/S field difference	typical N/S field integral difference
isostatically pressed blocks (old)	several %	up to 20 %
die-pressed blocks (new)	0.5 %	0.5 %

## Present material specifications

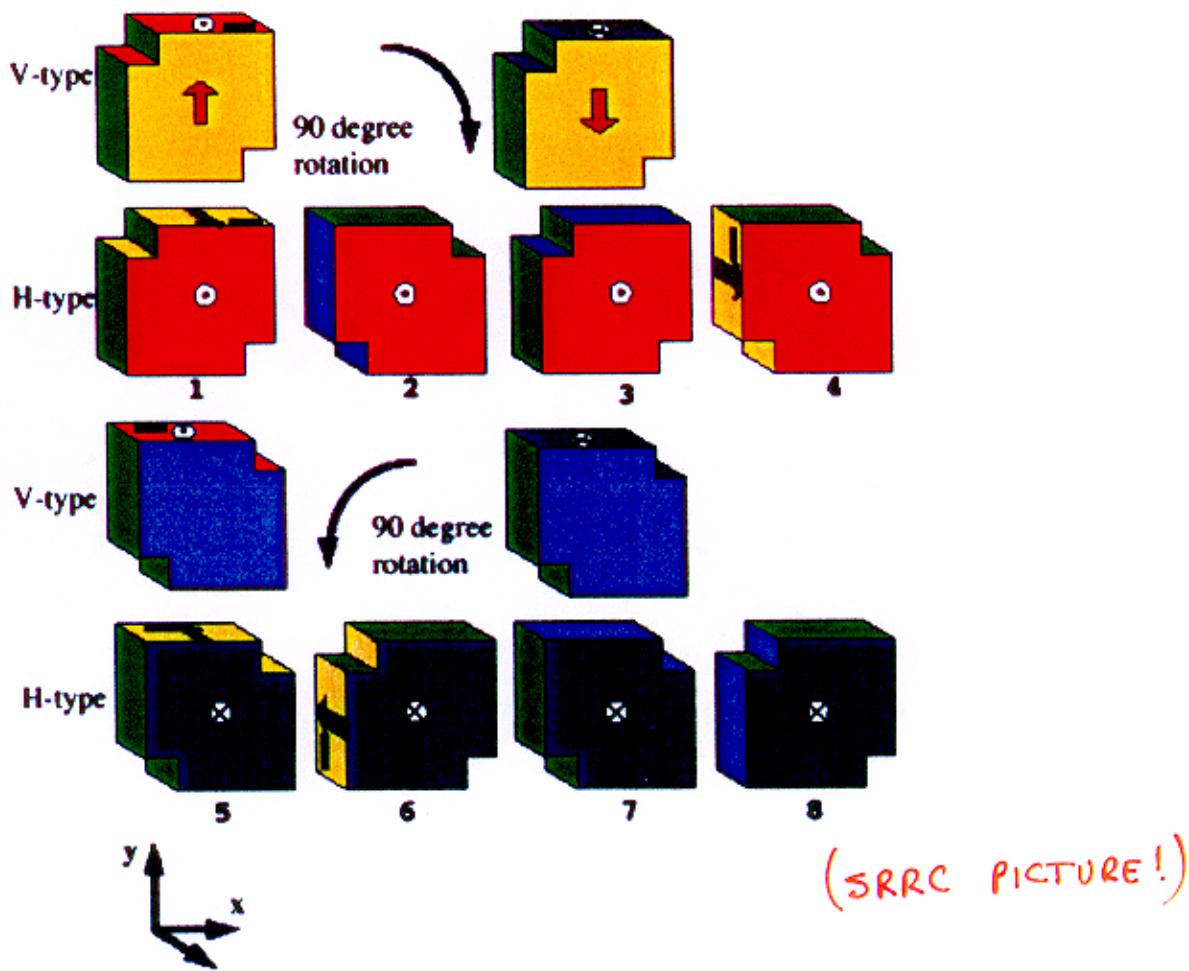
Remanent field	> 1.3 T
Dipole moment	$\pm 0.5\%$
Angle	$\pm 1^\circ$
N/S rel. field diff.	0.5 %

## *Sorting and shimming techniques for circularly polarizing permanent magnet undulators*

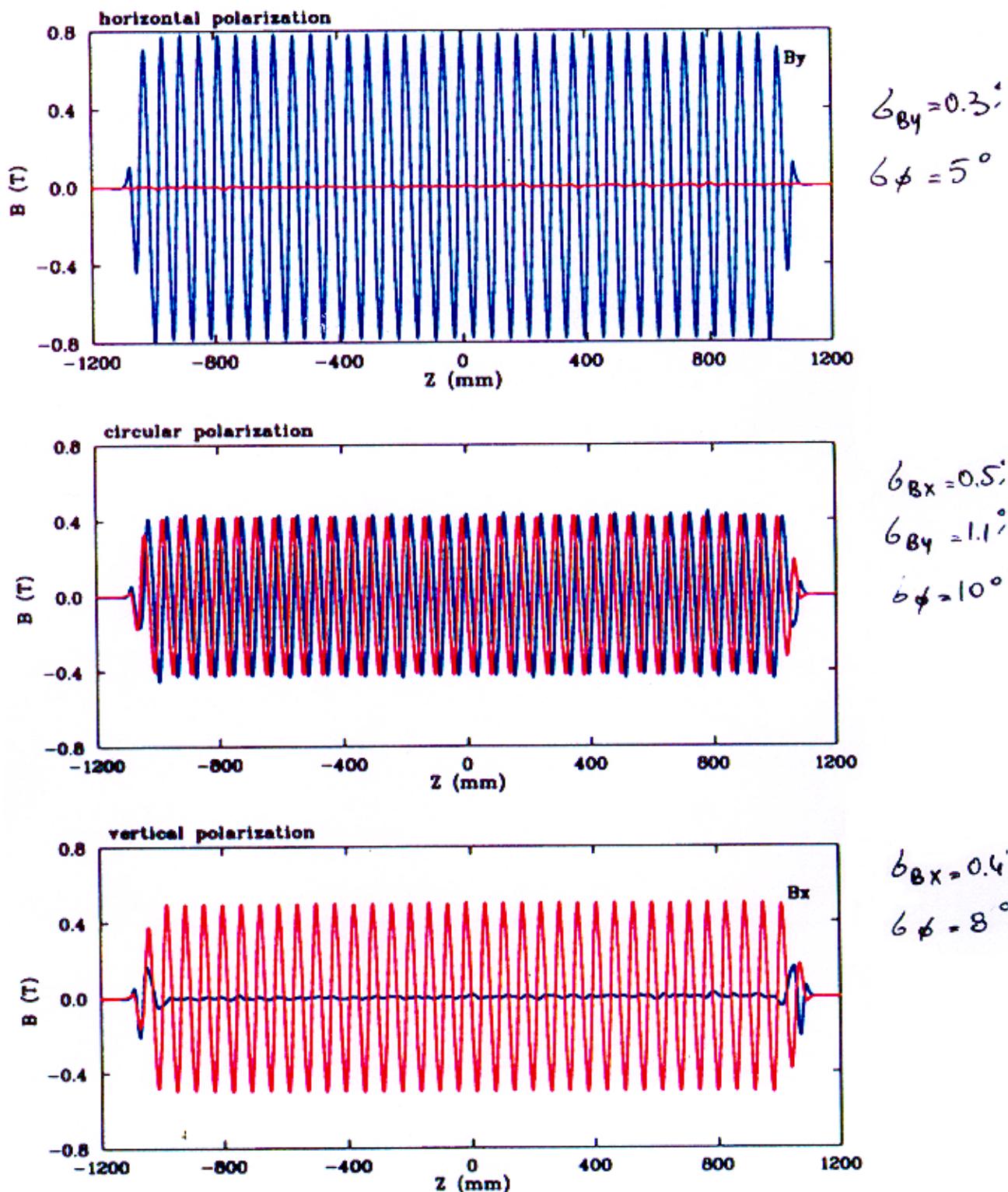
Sorting based on magnetization data (i.e. assuming homogeneous magnetization) has been used for the first time with good results

Simulated annealing algorithm optimizes for:

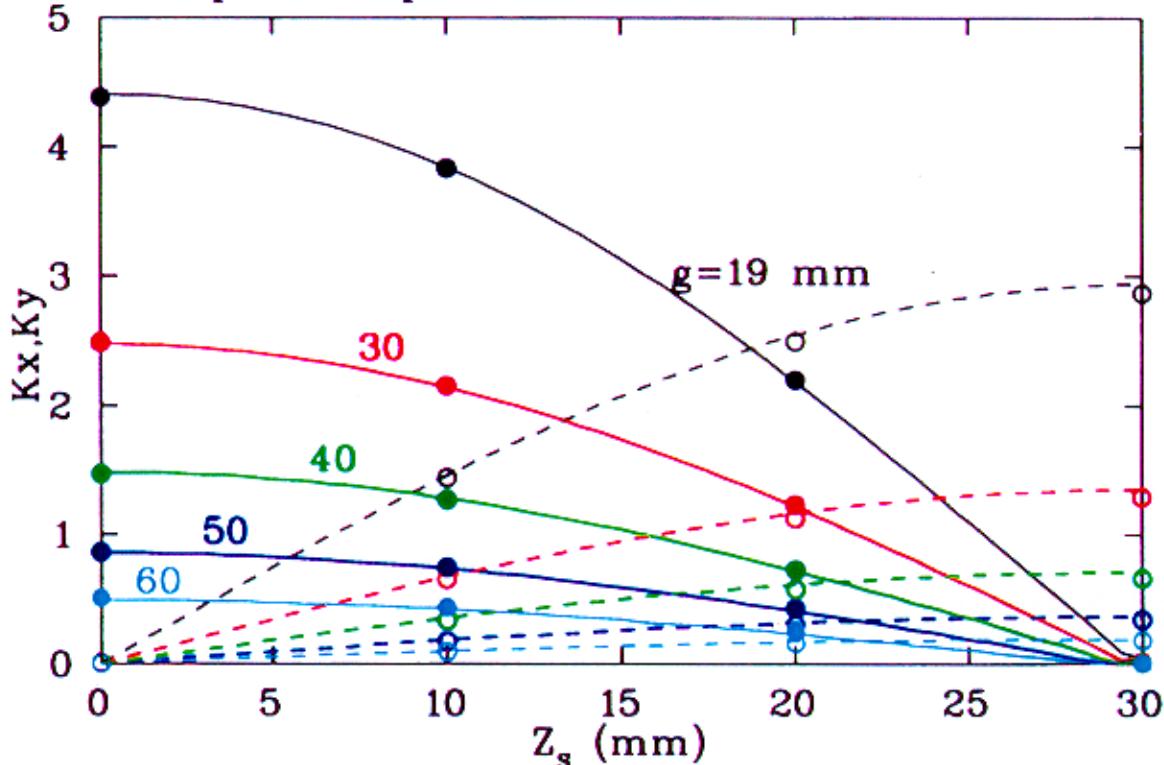
- rms optical phase error
- first and second field integral at  $x=0$
- first and second field integral off-axis distribution



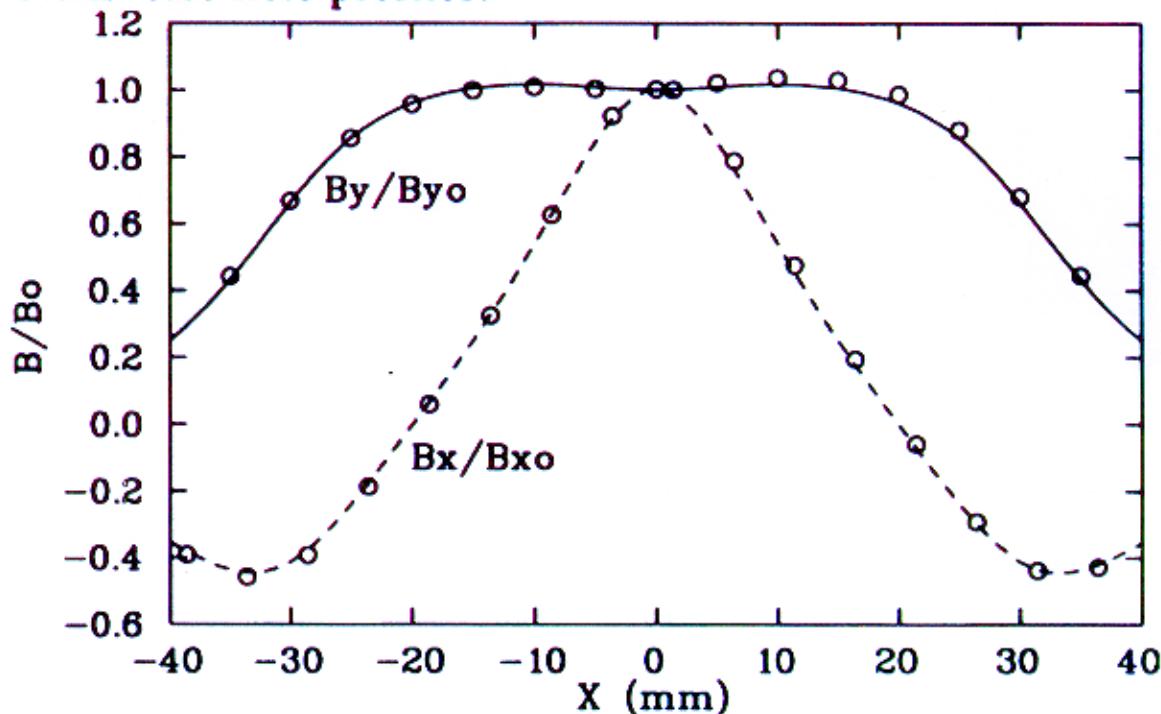
# Measured field at 19 mm gap in various polarization modes:



## Measured/predicted peak field:



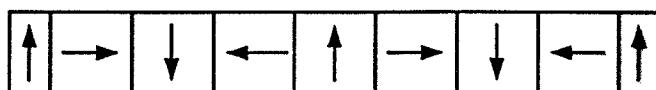
## Transverse field profiles:



# DESIGN OF TERMINATIONS

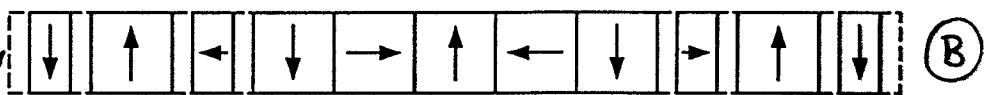
## FOR PPM UNDULATORS

STANDARD



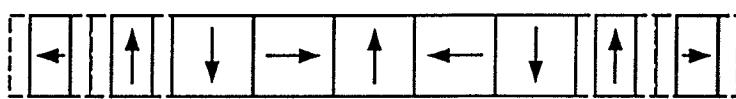
(A)

ELETTRA  
EPV 6.0/12.5



(B)

DISPLACEMENT  
FREE

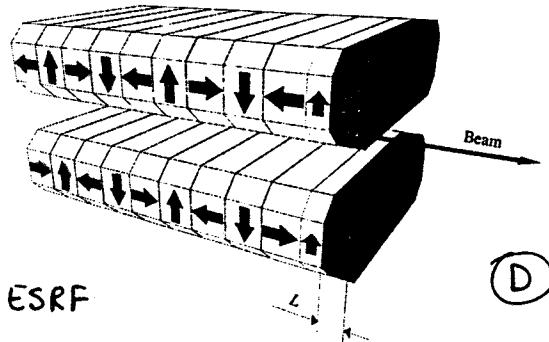


(C)

SERC  
EPV 5.6 ?

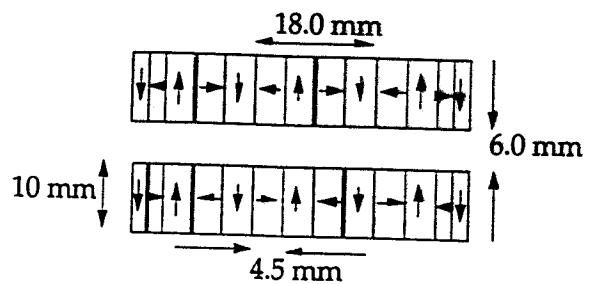


(E)

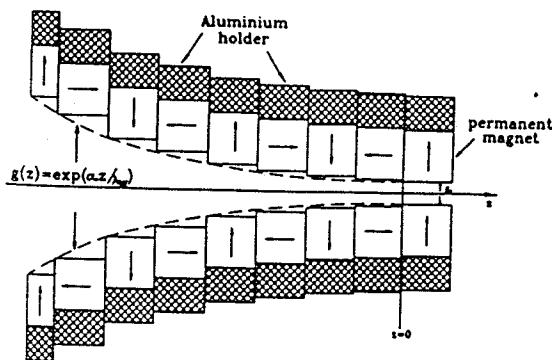


ESRF

(D)



SLAC/BNL/LBL VISA UNDULATOR



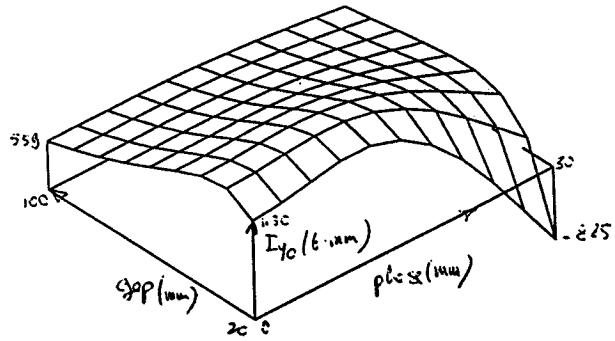
NEARLY  
DISPLACEMENT  
FREE

Fig. 2. Geometrical structure of an adiabatic end tapering.

$\mu \neq 1$  EFFECTS

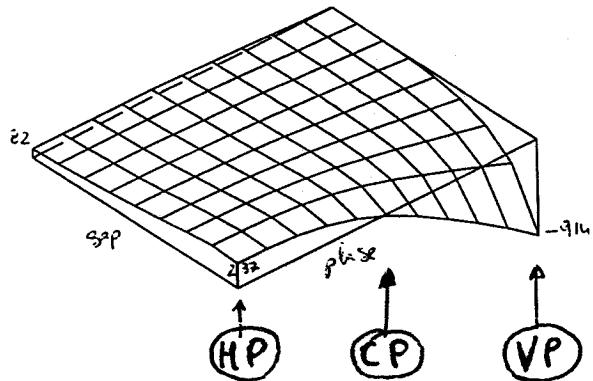
( $\mu_{||} = 1.05, \mu_{\perp} = 1.15$ )

LEPV6.0J



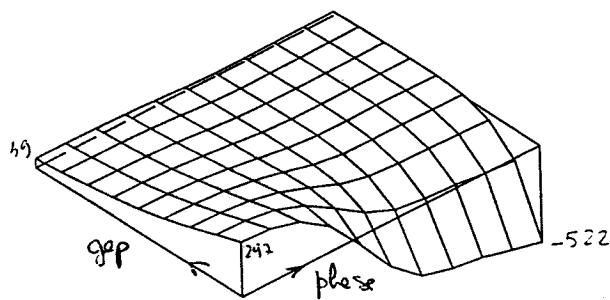
(A)

STANDARD  
TERMINATION



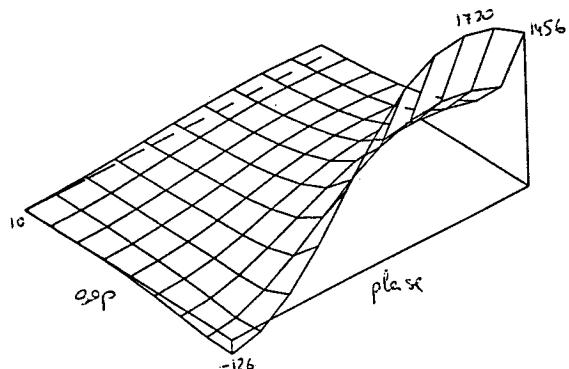
(B)

- Reduced DI<sub>y</sub> (gap)
- Reduced DI<sub>y</sub> (phase)  
(particularly between HP and CP)



(C)

- Reduced DI<sub>y</sub> (gap)
- "Fast" variation with phase



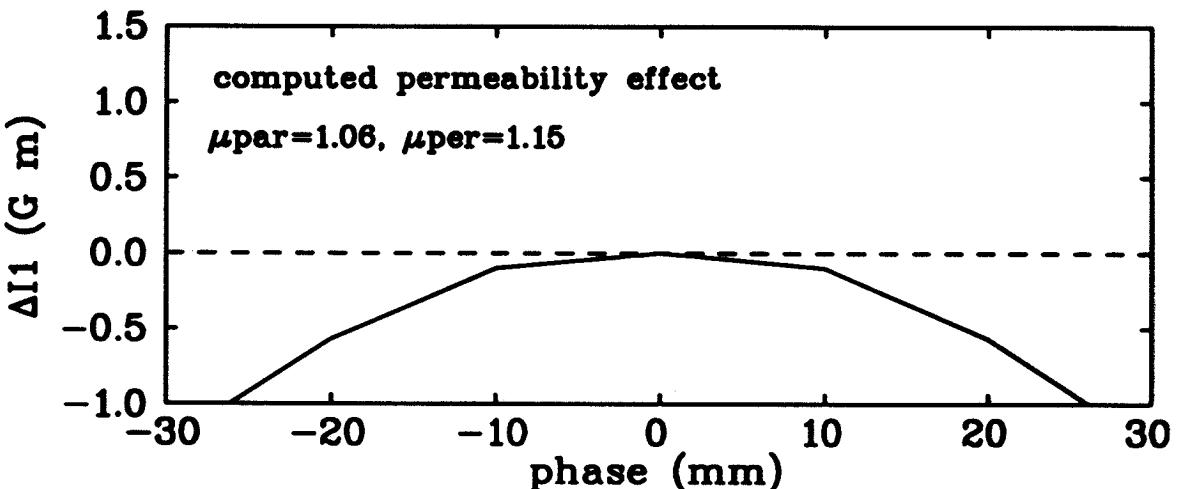
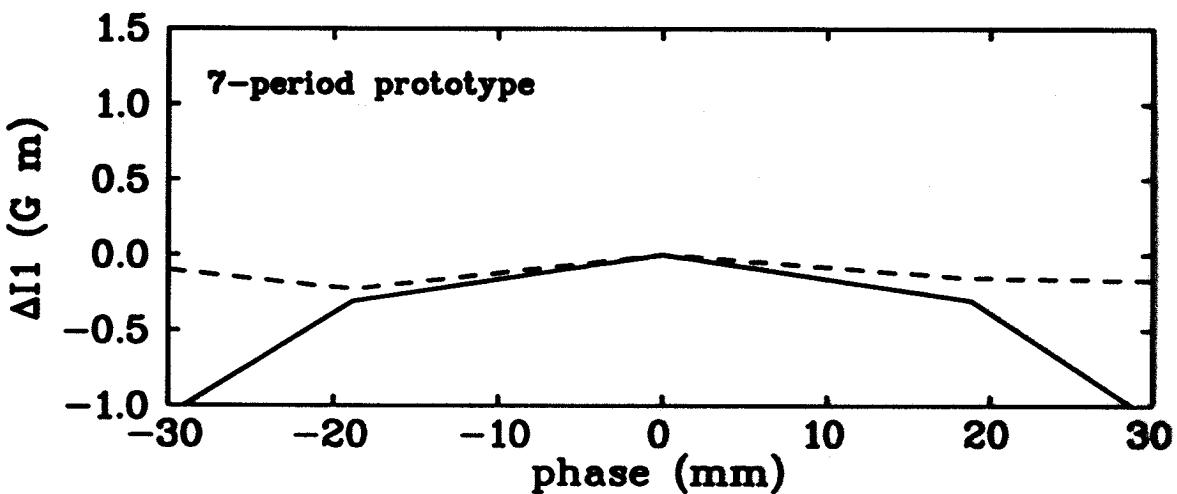
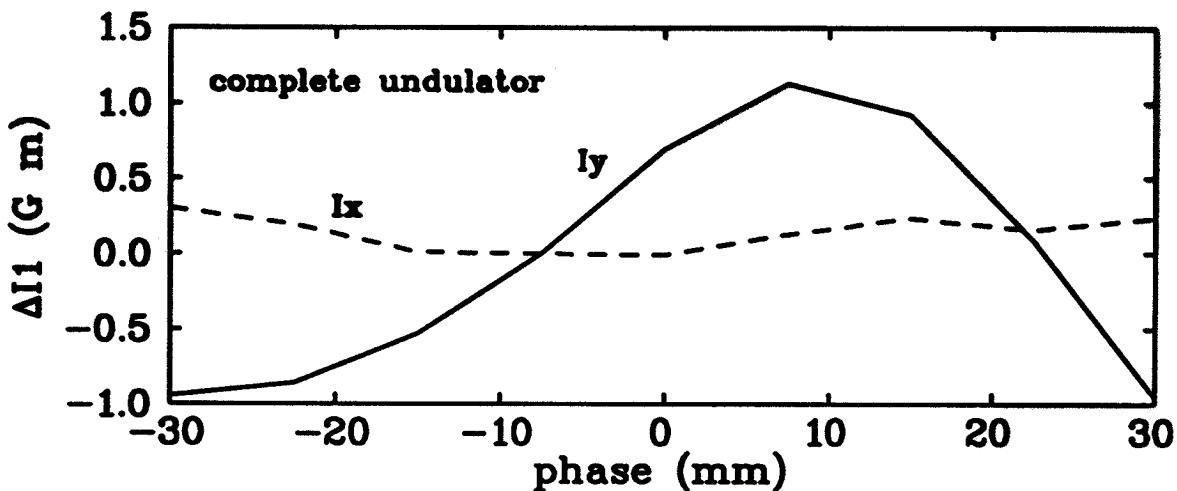
(D)

- Nearly zero DI<sub>y</sub> (gap)
- Large and "fast"  
variation with the phase

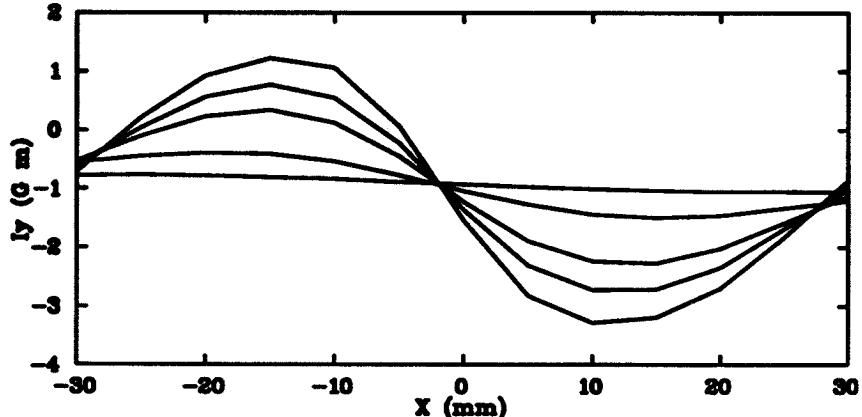
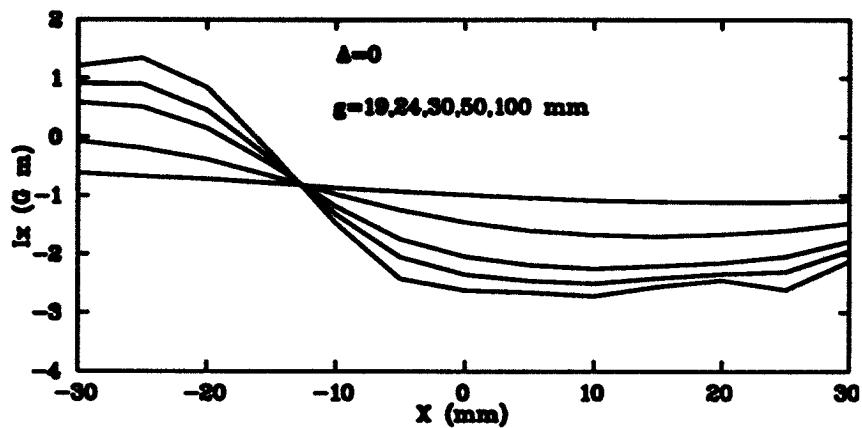
ALSO TO CONSIDER :

- FRINGE FIELD AMPLITUDE
- RAMP-UP TO FULL FIELD

# Variation of field integrals with the phase



Measured field integrals transverse distribution is dominated by a (~phase independent) quadrupole error (300 G):

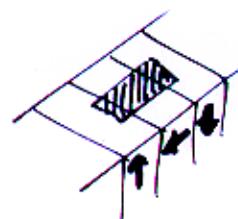
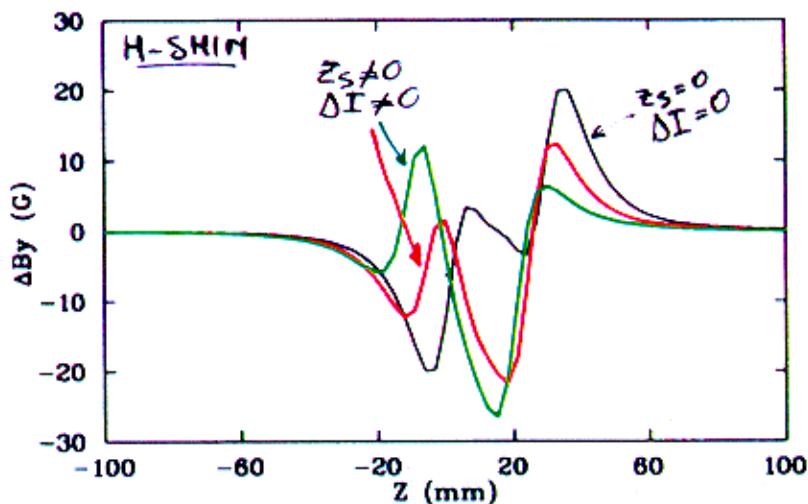
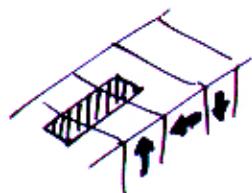
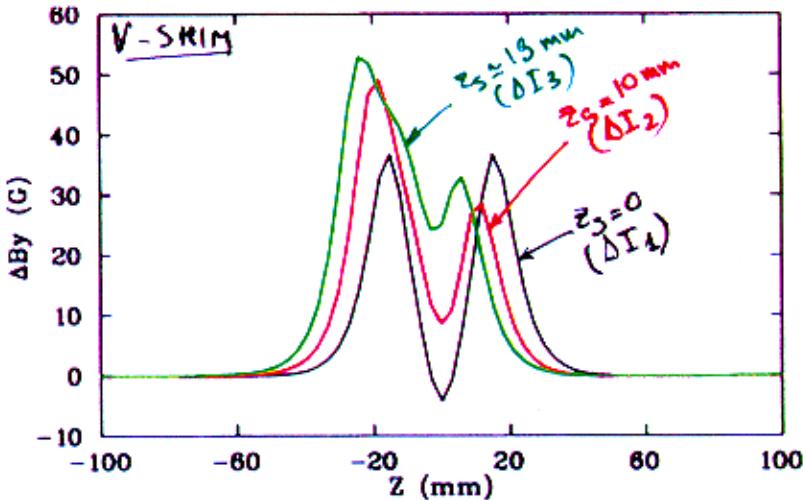


## Shimming

Conventional shimming method is complicated by the strong dependence of the shimming effect on the phasing of the arrays.

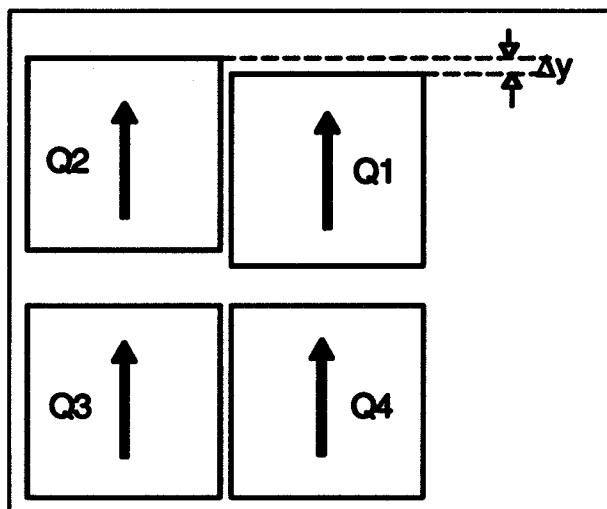
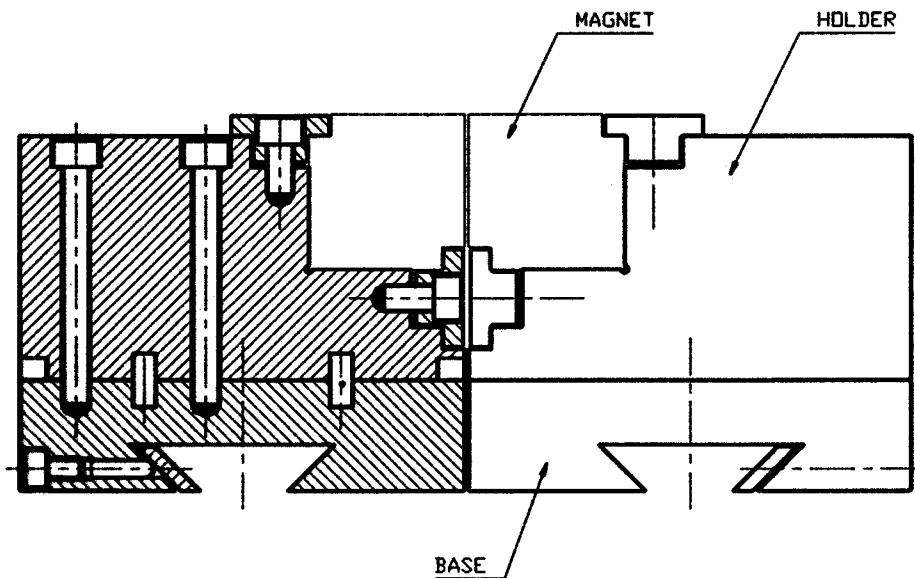
Usual distinction between V-shim and H-shim is no more applicable in the variable polarization case.

V-Shim and H-shim on-axis 'signatures' for linear, elliptical and circular polarization modes:

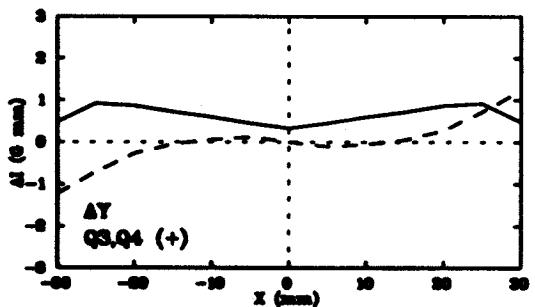
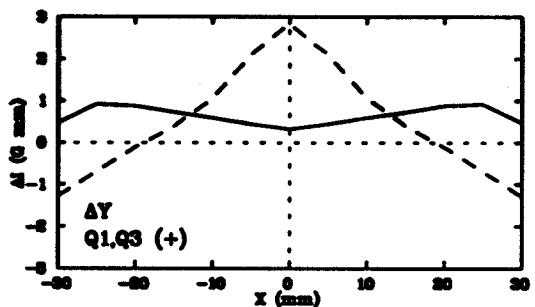
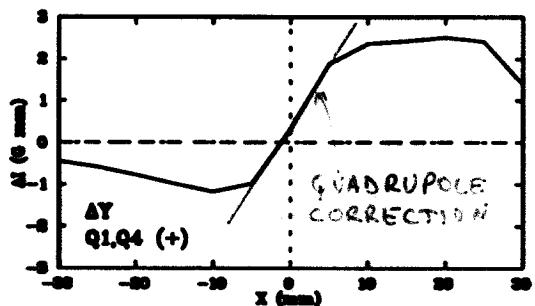
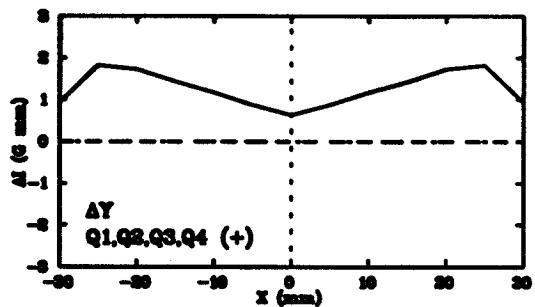
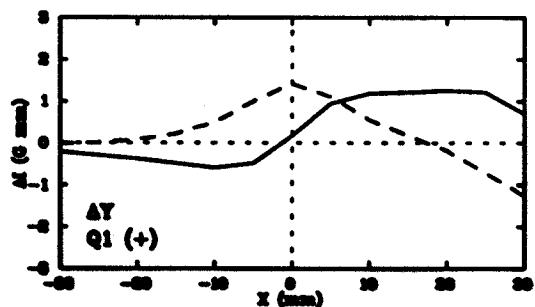


# Multipole errors correction by block displacement

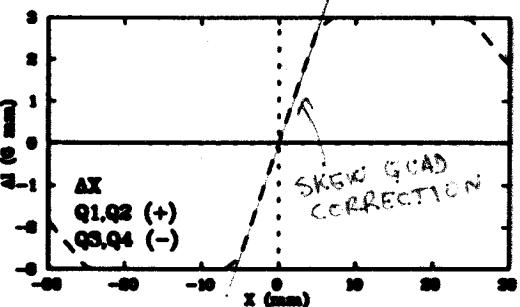
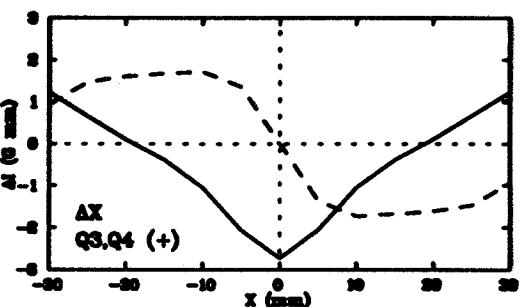
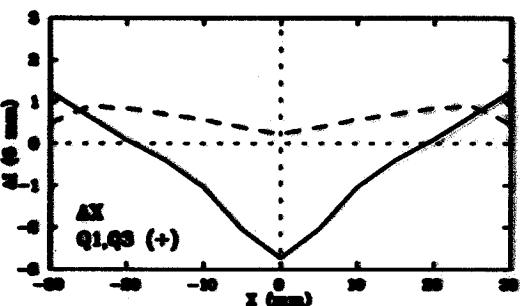
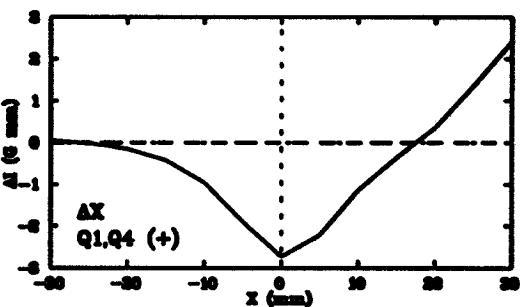
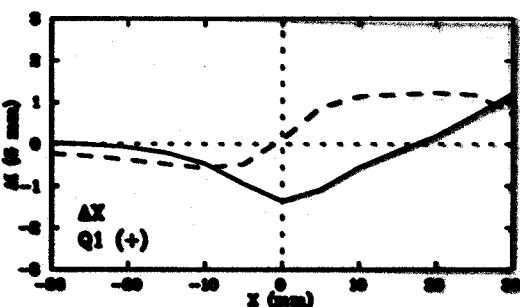
- Only vertical displacements are allowed with the present block holder design



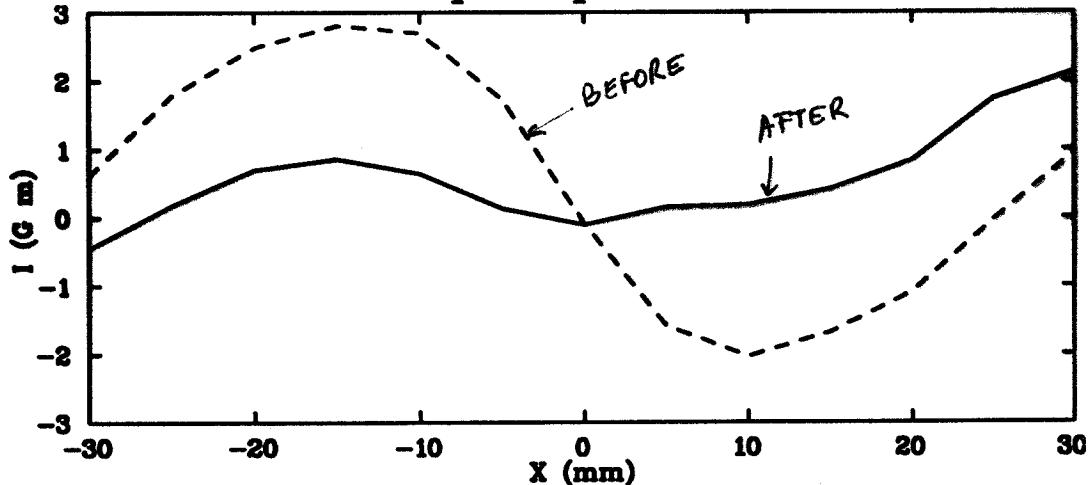
VERTICAL DISPLACEMENT  
( $\Delta Y$ )



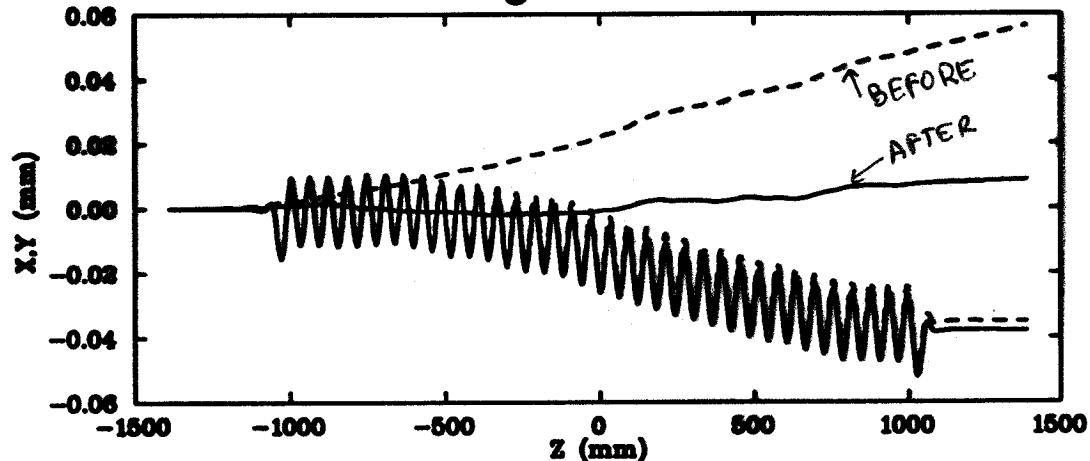
HORIZONTAL DISPLACEMENT  
( $\Delta X$ )



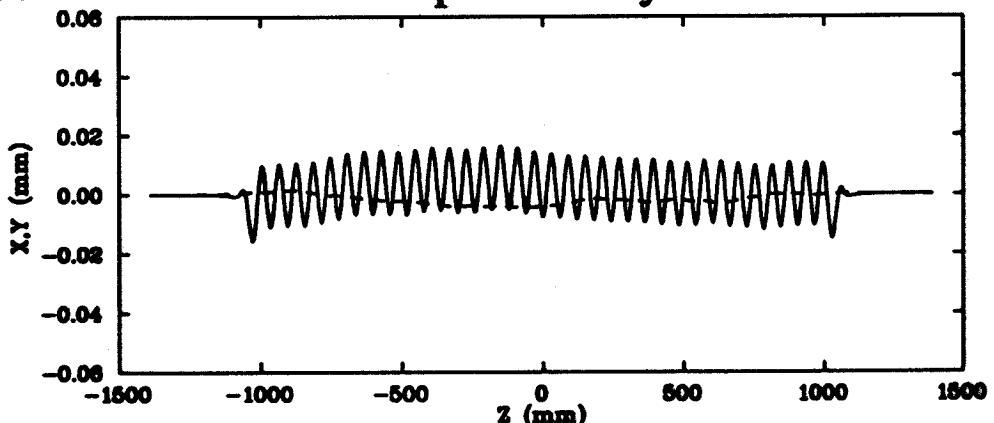
## Correction of vertical quadrupole error...



...is achieved simultaneously with reduction of horizontal first and second field integrals



residual effect will be compensated by correction coils:

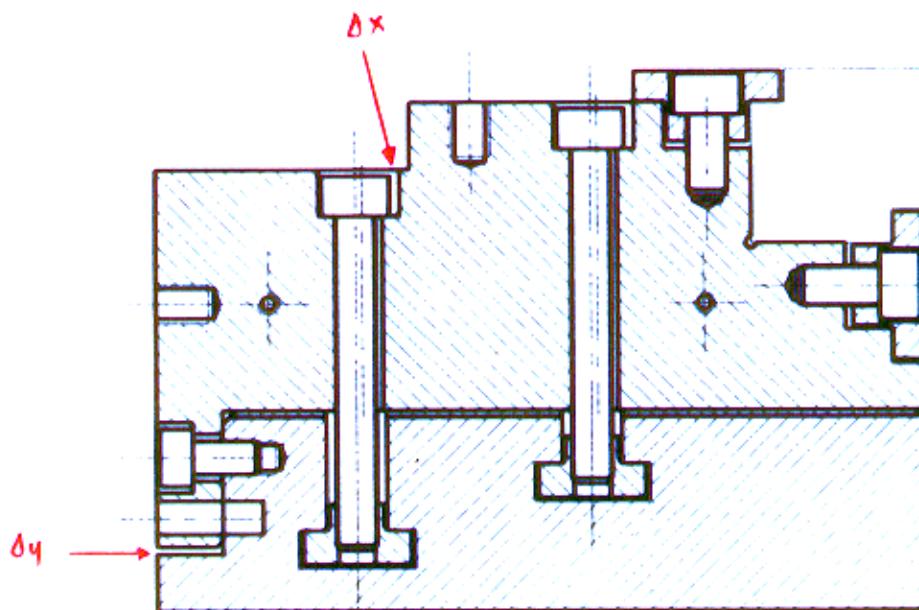


## Measured skew and normal integrated quadrupole and sextupole errors after correction

gap (mm)	phase (mm)	Qx (G)	Sx (G/cm)	Qy (G)	Sy (G/cm)
19	-20	-129	-9	13	206
19	-10	-105	-40	-34	150
19	0	-61	-67	-15	90
19	10	-50	-71	43	57
19	20	-104	-47	76	139
30	0	-51	-14	-7	26
50	0	-33	13	1	-1

ERRORS BECOME  
SMALLER AT LARG  
GAPS. INHOMOGENEITY

Improvements: new block holder allowing both horizontal and vertical displacement from the nominal position

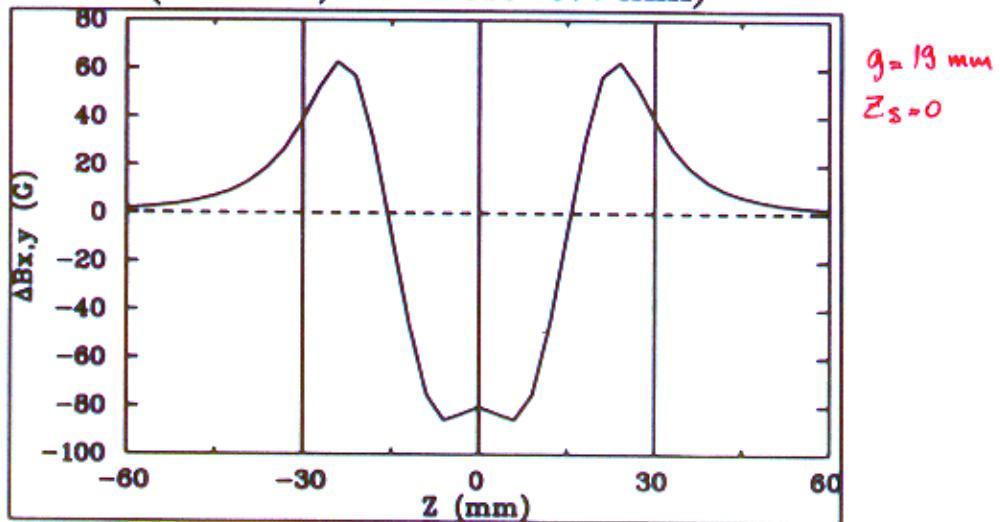


## Phase Shimming

- Basic shimming unit consists of 2 or 4 shims placed on consecutive H-blocks

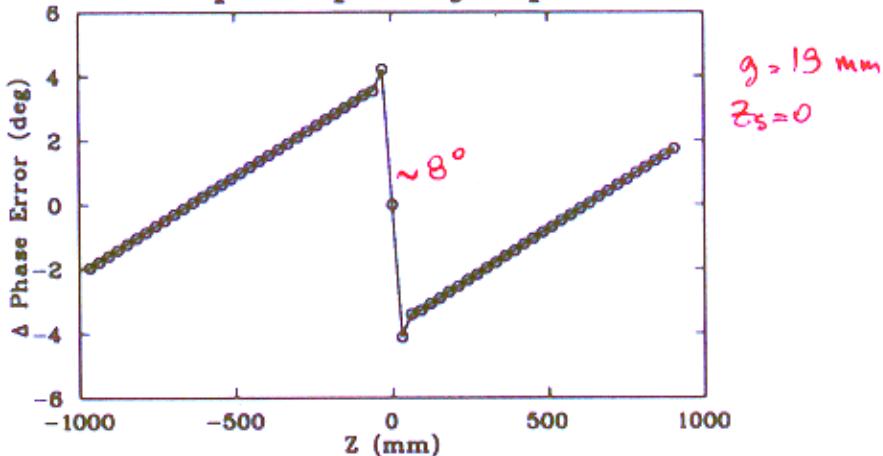


Computed field perturbation  
(4-shims, thickness=0.4 mm)

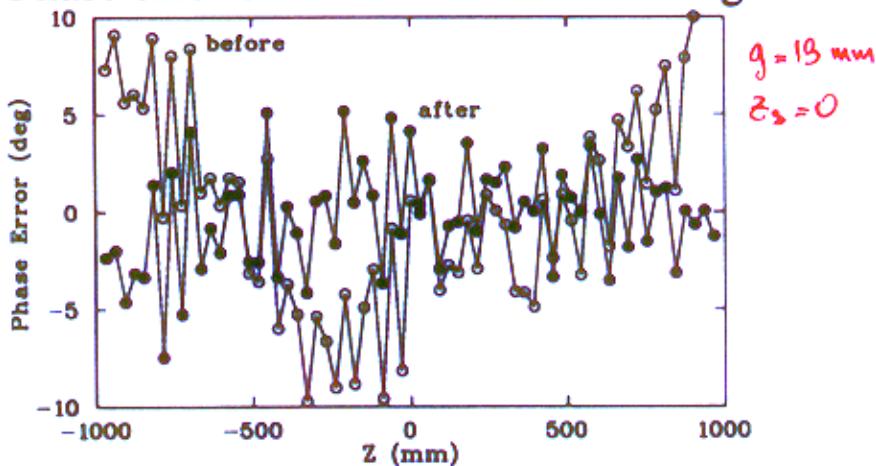


- The net effect on field integral is cancelled within the unit

## Optical phase jump



## Phase error before and after shimming

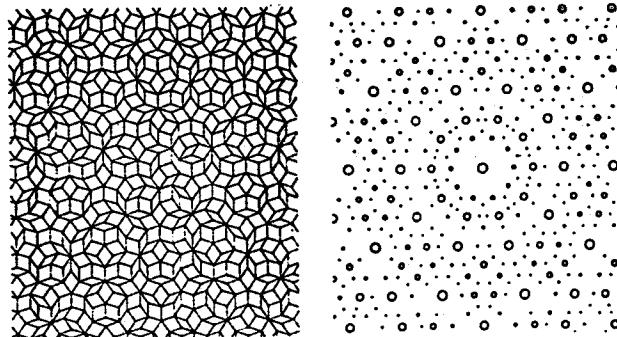


## Rms phase error as a function of phase at 19 mm gap

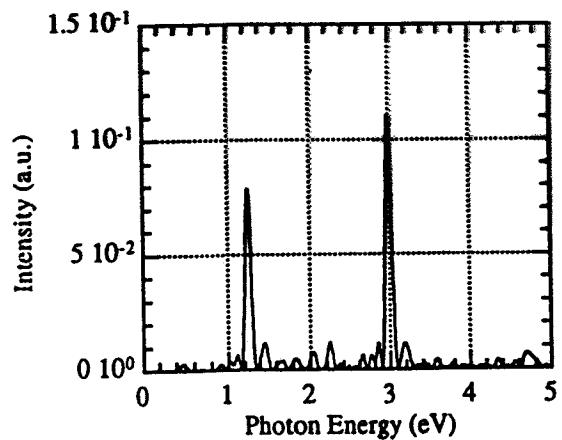
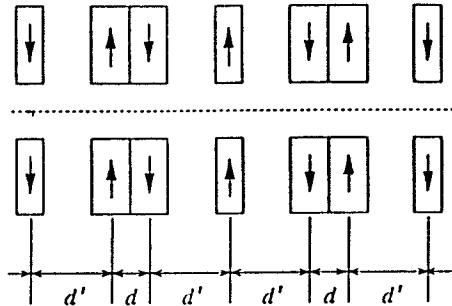
$z_s$ (mm)	polarization mode	$\sigma_\phi$ ( $^\circ$ ) before shimming	$\sigma_\phi$ ( $^\circ$ ) after shimming
-20	circular	8.0	4.9
-10	elliptical	4.6	4.2
0	horizontal	4.5	2.3
10	elliptical	7.2	2.6
20	circular	10.0	4.8

## Quasi periodic undulator

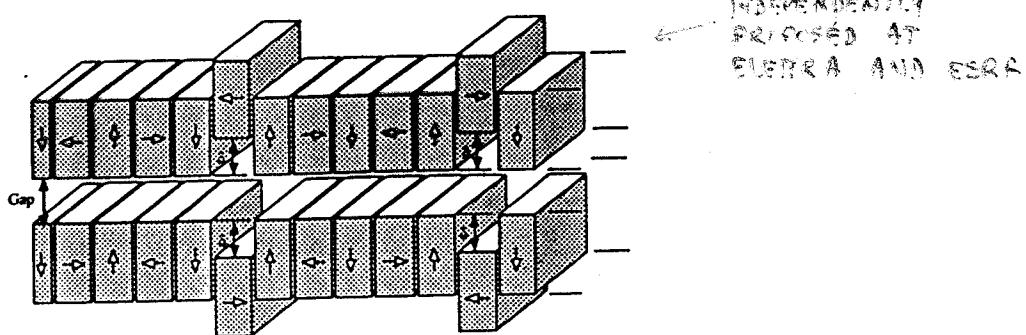
Diffraction from quasi-periodic crystals  
↓  
5/10-fold symmetry



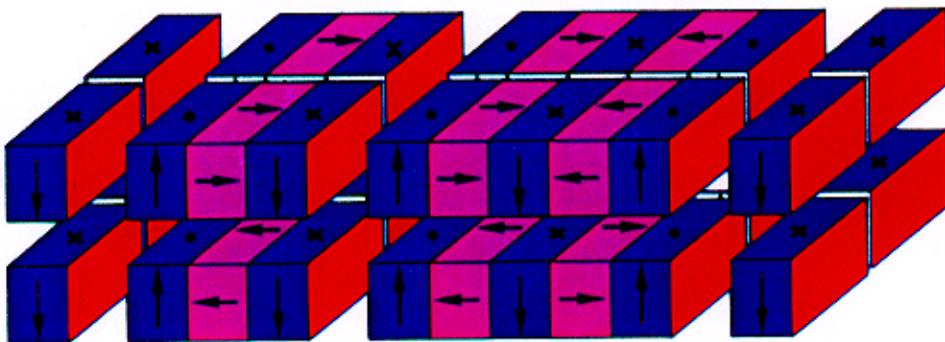
Quasi periodic sequence of pole separations  
↓  
non-harmonic spectrum



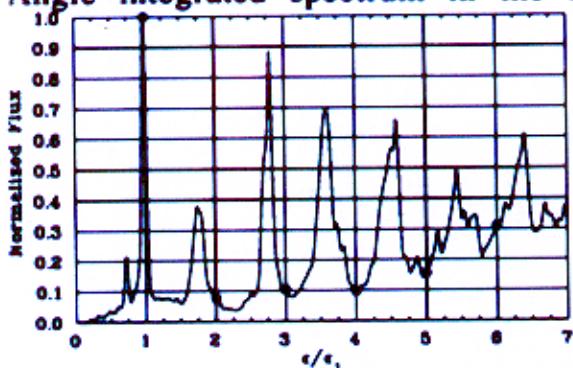
New concept: apply quasi-periodic sequence to field amplitude



# Quasi-periodic variable polarization undulator



Angle integrated spectrum in the linear ...



...and circular polarization mode

